

110°C dry

wet

Sample	wt.	pap. corr.	corr. wt.	crucible	cr. + samp.	samp. g	cr. + samp.	samp.	$S_w - S_d = \Delta$	$\frac{\Delta}{\sum} = \% H_2O$	cont. wt. x dry = wt. H ₂ O = H ₂ O cont.
A-1				6.4576	6.5591	.1015	6.5579	.0953	.6062	6.11	
gyre 82-11				6.3138	6.4123	.0985	6.4103	.0965	.602	2.03	
Dredge Composite		Phosph.		6.4743	6.5753	.1010	6.5720	.0977	.0033	3.27	
gyre 82-11 Dredge 4-Composite D-4		Phosph-carb		6.4288	6.5420	.1132	6.5401	.1113	.0019	1.68	
gyre 82-11 Dredge Composite C-6		Phosph.		6.2328	6.3096	.0768	6.3069	.0741	.0017	3.52	
gyre 82-11 D-8		Phosph/mn coatings		6.7828	6.8810	.0982	6.8779	.0951	.0031	3.16	
gyre 82-11 D-9		Phosph/MN		7.7198	7.8044	.0846	7.7964	.0766	.006	9.46	
gyre 82-11 D-10		Nodule/slc		6.6493	6.7506	.1013	6.7440	.6947	.0066	6.52	
gyre 82-11 D-11		Nodule		6.4545	6.5248	.0703	6.5202	.0657	.0046	6.54	
gyre 82-11 D-12		has Phosph. CARB		7.7254	7.8121	.0867	7.8103	.49	.0018	2.08	
gyre 82-11 D-14		MN-P plates		7.4900	6.5772	.0872	6.5712	.0812	.006	6.88	
gyre 82-11 D-15		MN slabs some carb		6.8674	6.9372	.0698	6.9336	.0662	.0036	5.16	
gyre 82-11 D-16		CARB	7	6.8116	6.9079	.013	6.9062			3.12	
gyre 82-11 D-17				10.8090	10.8838				.8	2.41	
gyre 82-11 D-18				9.3520	9.47		.0696		.0012		

dry

wet

Sample	wt.	pop. corr.	corr. wt.	crucible	cr. + samp.	samp.	cr. + samp.	samp.	$S_w - S_d = \Delta$	$\frac{\Delta}{S_w} = \% H_2O$	cont. of vol. $H_2O = wt. H_2O$	cont. wt. - wt. H_2O cont.
NYC 82-11 Dredge Composite D-5	1000°	Phosph CARD		9.8290	9.9105	.0815	9.9958	.0768	.0047	5.77		
NYC 82-11 Dredge Composite 9 82- D-10		CONT. WT MANFE 51A B		10.0127	10.0992	.0865	10.0972	.0845	.0027	2.31		
D-10				9.4212	9.5044	.0832	9.4962	.075	.0082	9.86		
C				9.1436	9.2049	.0613	9.1988	.0552	.0061	9.95		
E				9.7839	9.8544	.0705	9.8474	.0635	.007	9.93		
F				9.3196	9.3838	.0642	9.3779	.0583	.0059	10.12		
G				9.4221	9.4897	.0676	9.4833	.0612	.0064	9.47		
H				11.3052	11.3749	.0697	11.3692	.064	.0057	8.18		
I				9.4603	9.5524	.0921	9.5454	.0851	.007	7.60		
J				7.7431	7.8215	.0784	7.8155	.0724	.0060	7.65		
K				6.8197	6.8747	.0550	6.8700	.0502	.0047	8.55		
R	Bermuda Rise			6.4727	6.5383	.0656	6.5351	.0624	.0032	4.88		
BA				6.6581	6.6581							

$$\text{Let } C_{12} = C_{11}/C_3$$

$$C_8 = C_4 - C_2$$

$$2 \epsilon_i \frac{.0291}{.0865} C_4 - C_2$$

C-11

C₃

Total
500°C

C₁
110°C

C₄
1000°C

C₈
Ca

Sample #	Mn %	Fe %	Mn + Fe	Total 500°C	C ₁ 110°C	C ₄ 1000°C	C ₈ Ca
D-1	.2514	8.8	9.05	5.69	2.03	15.74	21.6
D-2	.029	1.33	1.36	2.67	2.41	29.71	24.2
D-3	.032	1.57	1.60	3.67	1.69	26.97	23.0
D-4	.071	4.95	5.02	6.83	3.27	18.61	24.6
D-5	6.72	10.96	17.68	10.06	5.77	25.44	18.4
D-8	6.87	19.3	26.17	11.20	3.52	22.79	13.6
D-9	17.08	11.51	28.59	17.26	9.46	30.85	10.7
D-10	12.35	8.2	20.55	13.13	6.52	33.46	16.9
D-11	13.73	10.6	24.33	14.79	6.54	33.00	16.2
D-12	1.99	8.34	10.33	6.34	2.08	22.95	17.6
D-14	13.43	13.32	26.75	14.68	6.88	32.57	13.3
D-15	10.22	8.9	19.12	11.75	5.16	34.36	17.9
D-16	.029	.150	0.179	3.53	.312	44.62	22.2
D-17	1.77	.569	2.34	5.78	2.31	33.64	24.2
C-6	.814	2.96	3.77	3.80	1.68	23.06	22.3
C-9	5.93	4.42	10.35	7.13	3.16	25.05	23.1
A-1	17.53	10.34	27.87	14.09	6.11	28.87	10.9
R (Bermuda Rise)				13.57	4.88		

no bus
show good
to hit target
m = 2.156
b = -5.498

$$P_h = \frac{A}{D^2} \text{ Por(Mn+Fe)}$$

good
Math Good
1979
Can
C. Ching
$$\text{Por}_{1000^\circ} = \text{Por}_{\text{Fe-Mn}} + \text{Por}_{\text{CO}_2}$$

$$\text{Por}_{\text{CO}_2} \text{ corr Ca}$$